A Numerical Algorithm for the Solution of Viscous Incompressible Flows on GPUs

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Due to the difficulty on solving exact N-S equations, numerical schemes have been adopted to solve complex fluid flows patterns. The most popular being F*M (for FDM, FVM or FEM). In particular, FDM/FVM method on structured grids are very suitable to solve on GPGPU's due to the local requirement of data to solve the fields (Cellular automata¹).

Our concern is

- a quick method in order to make real time computation, and also
- having enough precision to solve engineering problems.

The equations governing incompressible Newtonian fluid flows are

$$\begin{aligned} \frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} &= -\frac{1}{\rho} \nabla \rho + \nu \Delta \mathbf{u} + \rho \mathbf{f}_e \\ \nabla \cdot \mathbf{u} &= 0 \end{aligned} \tag{1}$$

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being

- **u**: velocity,
- ρ : density,
- *p*: pressure,
- ν : kinematic viscosity,
- **f**_e: body forces per volume unit.

In order to solve the momentum equations in (1)

- Artificial compressibility,
- Fractional steps (\longrightarrow FFT).

So the process is basically a splitting, considering Forward Euler time integration the two equations are

$$\frac{\mathbf{u}^* - \mathbf{u}^n}{\Delta t} = -\nabla \cdot (\mathbf{u} \otimes \mathbf{u})^n + \nu \Delta \mathbf{u}^n$$
(2)

$$\frac{\mathbf{u}^{n+1} - \mathbf{u}^*}{\Delta t} = -\frac{1}{\rho} \nabla p^{n+1} \tag{3}$$

namely, the former having convective-diffusive terms and the later the pressure.

Fractional-Step Method

The Fractional-step has three steps

- 1 solving (2) (predictor step),
- 2 solving a Poisson equation for pressure

$$\Delta p^{n+1} = \frac{\rho}{\Delta t} \left(\nabla \cdot \mathbf{u}^* \right), \tag{4}$$

3 updating \mathbf{u}^* (corrector step, equation (3)) and obtaining \mathbf{u}^{n+1} . Using Adams-Bashforth 2th order time integration, the momentum equations problem is

$$\mathbf{u}^* = \mathbf{u}^n + \frac{\Delta t}{2} \left[3R(\mathbf{u}^n) - R(\mathbf{u}^{n-1}) \right], \qquad (5)$$

where

$$R(\mathbf{u}^n) = -\nabla \cdot (\mathbf{u} \otimes \mathbf{u})^n + \nu \Delta \mathbf{u}^n.$$
(6)

Using centered schemes for the velocity and pressure in the velocity correction methods produces

- odd-even nodes decoupling equations on pressure and velocity and
- spatial decoupling between pressure and velocity.

Solution: \rightarrow Staggered Grids.

In order to get a *stable* solution for the convective terms, the QUICK approach is used. Its advantages includes

- truncation error O(δ³) on grids with a displacement of δ/2 (where δ = Δx, Δy, Δz, in order to represent the 3 spatial dimensions),
- mass conservation and other stability characteristics.

Solving the Linear System

- We have to solve a linear system $\mathbf{A}\mathbf{x} = \mathbf{b}$
- The Discrete Fourier Transform (DFT) is an orthogonal transformation \$\tilde{x} = Ox = fft(x)\$.
- The inverse transformation $\mathbf{O}^{-1} = \mathbf{O}^T$ is the inverse Fourier Transform $\mathbf{x} = \mathbf{O}^T \tilde{\mathbf{x}} = \operatorname{ifft}(\mathbf{x})$.
- If the operator matrix A is *homogeneous* (i.e. the stencil is the same at all grid points) and the b.c.'s are periodic, then it can be shown that O diagonalizes A, i.e. OAO⁻¹ = D.
- So in the transformed basis the system of equations is diagonal

$$(\mathbf{OAO}^{-1})(\mathbf{Ox}) = (\mathbf{Ob}),$$

$$\mathbf{D\tilde{x}} = \tilde{\mathbf{b}},$$
 (7)

• For $N = 2^p$ the Fast Fourier Transform (FFT) is an algorithm that computes the DFT (and its inverse) in $O(N \log(N))$ operations.

Solving the Linear System

- So the following algorithm computes the solution of the system in O(N log(N)) ops.
 - $\tilde{\mathbf{b}} = \operatorname{fft}(\mathbf{b})$, (transform r.h.s)
 - $\tilde{\mathbf{x}} = \mathbf{D}^{-1}\tilde{\mathbf{b}}$, (solve diagonal system O(N))
 - $\mathbf{x} = \operatorname{ifft}(\tilde{\mathbf{x}})$, (anti-transform to get the sol. vector)
- Total cost: 2 FFT's, plus one element-by-element vector multiply (the reciprocals of the values of the diagonal of D are precomputed)

- In order to precompute the diagonal values of **D**,
 - We take any vector \mathbf{z} and compute $\mathbf{y} = \mathbf{A}\mathbf{z}$,
 - then transform $\tilde{z} = \operatorname{fft}(z)$, $\tilde{y} = \operatorname{fft}(y)$,

$$\bullet D_{jj} = \tilde{y}_j / \tilde{z}_j.$$

Solving the Linear System



- The system to be solved generally is quite large.
- It can be seen that our domain is compose on fluid and solids.
- The Poisson solver gets *a very approximate* solution of the pressure field.
- In order to take into account the boundary condition an iterative method (CG+FFT) is used.

It can be shown that the condition number of the preconditioned system remains constant with refinement.

Evolution of the condition number



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LDC Test - Simple Precision



Cube Test - Simple Precision



Sphere Test - Simple Precision



GPGPU Results



CPU Results

- i7-3820@3.60Ghz (Sandy Bridge), 1 core (sequential):
 1.7 Mcell/sec
- i7-950@3.07 (Nehalem), 1 core (sequential): 1.51 Mcell/sec
- Cellrates with nthreads>1, and W3690@3.47Ghz not available at this time.

 BUT, we expect at most 7 to 10 Mcell/secs, so there is speedup factor of 8 to 10, with respect to the GPGPU (GTX-580, DP).

Results analysis

- For a 128×128×128 mesh (≈ 2Mcell), we have a computing time of 2 Mcell/(140 Mcell/sec) = 0.014 secs/time step.
- That means 70 steps/sec.
- A von Neumann stability analysis shows that the QUICK stabilization scheme is unconditionally unstable if advanced in time with Forward Euler.
- With a second order Adams-Bashfort scheme the critical CFL is ≈ 0.588 (pure advection).
- For NS eqs. the critical CFL has been found to be somewhat lower (≈ 0.5).
- If L = 1, u = 1, h = 1/128, $\Delta t = 0.5h/u = 0.004$ [sec], so that we can compute in 1 sec, 0.28 secs of simulation time. We say ST/RT=0.28.

Steps computing times



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Considerations

- It can be seen on the previous image that the momentum equations are being solved in the same amount of time that the Poisson step.
 - Problem: QUICK Too much shared memory and/or registers used (other methods are being tested).
- The sphere test show a very rough surface; currently refinement approaches are being tested but far from be fully programmed and tested.

• Possible Problem: Poor drag computation².

Flow around a cylinder shown good³ Strouhal prediction (.259 at Re = 1000), but drag was not actually computed.

²More over, no boundary layer refinement is being done.

³Exp: 0.22, PFEM-2: 0.2475, Mittal= 0.25, OpenFOAM: 0.26.

Considerations



- Preliminary results shows that the flow is being *accelerated*, in comparison to the reference data (Ghia et al. 1998).
- Other stabilization schemes are being tested.

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Size: 2x512x512.

Conclusions



- QUICK method produces inefficiency due to a highly spread stencil (Too low flops/word relationship). Also, it seems like some artificial acceleration is being added.
- Staircase bodies reduce convergence and affect computation of drag forces.
- The speedup achieved, in comparison to a CPU, being 10-20x on SP and 7-10 on DP.

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